

GEOTECHNICAL INVESTIGATION

FOR

NSW Land & Housing Corporation

10 – 16 Albert Street, Casino

Report No: 22/3050

Project No: 31897/6742D-G

September 2022



Table of Contents

| 1. | INTR | ODUCTION | 2 |
|----|------|-------------------------------|-----|
| | | | |
| 2. | NAT | URE OF THE INVESTIGATION | . 2 |
| 2 | 2.1. | Fieldwork | . 2 |
| 2 | 2.2. | Laboratory Testing | . 3 |
| | | DLOGY AND SITE CONDITIONS | |
| 4. | SUB | SURFACE CONDITIONS | . 3 |
| 5. | GEO | TECHNICAL DISCUSSION | . 4 |
| | 5.1. | Site Classification to AS2870 | . 4 |
| | 5.2. | Foundation Design | . 4 |
| | 5.3. | Soil Aggressiveness | . 5 |
| 6 | FINA | AL COMMENTS | 6 |

DRAWING NO. 22/3050 – BOREHOLE AND PENETROMETER LOCATIONS
NOTES RELATING TO GEOTECHNICAL REPORTS

APPENDIX A - BOREHOLE LOGS AND EXPLANATION SHEETS

APPENDIX B – LABORATORY TEST RESULTS



1. INTRODUCTION

This report presents the results of a Geotechnical Investigation carried out by STS Geotechnics Pty Limited (STS) for a proposed new residential development to be constructed at 10 – 16 Albert Street, Casino. At the time of writing this report STS were not provided with architectural drawings for the project, however we understand the development will typically comprise the demolition of existing structures prior to construction of single or double storey residential buildings. The development will not include basement levels.

The purpose of the investigation was to:

- assess the subsurface conditions over the site,
- provide a Site Classification to AS2870,
- provide recommendations regarding the appropriate foundation system for the site including design parameters, and
- comment on soil aggressiveness to buried steel and concrete.

The investigation was undertaken at the request of NSW Land and Housing Corporation as outlined in STS's proposal referenced P22-433 dated July 27th, 2022.

Our scope of work did not include a contamination assessment.

2. NATURE OF THE INVESTIGATION

2.1. Fieldwork

The fieldwork consisted of drilling six (6) boreholes numbered BH1 to BH6, at the locations shown on Drawing No. 22/3050. The boreholes were drilled using a Christie drilling rig owned and operated by STS. Soil strengths were determined by undertaking Dynamic Cone Penetrometer (DCP) tests adjacent to each borehole location.

Drilling operations were undertaken by one of STS's experienced technical officers who also logged the subsurface conditions encountered.

The subsurface conditions observed are recorded on the borehole logs given in Appendix A. An explanation of the terms used on the logs is also given in Appendix A. Notes relating to geotechnical reports are also attached.

Project No: 31897/6742D-G

Report No: 22/3050



2.2. Laboratory Testing

To assess the soils for their aggressiveness, four (4) selective representative soil samples were tested to determine the following:

- pH,
- Sulphate content (SO₄),
- Chloride content (CL), and
- Electrical Conductivity (EC)

To assist with the site classification a representative soil sample was collected to determine their shrink swell index.

Detailed test reports are given in Appendix B.

3. GEOLOGY AND SITE CONDITIONS

The Tweed Heads geological series sheet at a scale of 1:250,000 shows that sandstone, siltstone, claystone, and coal belonging to the Grafton Formation underlies the site.

The site is roughly rectangular in shape with an area of approximately 3798 m². At the time of the fieldwork, the site was occupied by single storey houses.

Vegetation observed during fieldwork consisted of trees.

The ground surface falls about 1 metre south-east.

The site is bound by Albert Street to the east and single storey dwellings in the adjoining properties.

4. SUBSURFACE CONDITIONS

When assessing the subsurface conditions across a site from a limited number of boreholes, there is the possibility that variations may occur between test locations. The data derived from the site investigation programme are extrapolated across the site to form a geological model and an engineering opinion is rendered about overall subsurface conditions and their likely behaviour regarding the proposed development. The actual condition at the site may differ from those inferred, since no subsurface exploration programme, no matter how comprehensive, can reveal all subsurface details and anomalies, particularly on a site such as this that has been previously developed.

The subsurface conditions consist of topsoil overlying natural silty clays, sandy silty clays, silty clayey sands, clayey silty sands, clayey sands, and weathered rock. Topsoil was encountered from the surface to depths of 0.1 to 0.3 metres. Loose to medium dense silty clayey sands and clayey silty

Project No: 31897/6742D-G Report No: 22/3050



sands generally underlie the topsoil to depths of 0.4 to 0.6 metres. Soft to firm and firm to stiff, becoming very stiff with depth, silty clays, sandy clays, and sandy silty clays underlie the sands to the depth of auger refusal, 1.0 metre in BH3 and 1.2 metres in BH1, and to depths of 1.2 to 2.0 metres in the remaining boreholes. Weathered rock underlies the soils to the depths of auger refusal, 1.4 to 2.2 metres.

No groundwater was observed during the site drilling.

5. GEOTECHNICAL DISCUSSION

Site Classification to AS2870 5.1.

The classification has been prepared in accordance with the guidelines set out in the "Residential Slabs and Footings" Code, AS2870 – 2011.

To assist with determining the site classification, three (3) representative samples were retrieved from site for shrink swell testing. The detailed test report is attached and summarised in Table 5.1.

Table 5.1 – Shrink Swell Test Summary

| Location | Depth (m) | Material Description | Shrink/Swell Index (% per ∆pF) |
|----------|--------------|--|-----------------------------------|
| BH1 | 0.7 - 0.9 | Silty Clay: brown with orange, some fine | 2.0 |
| | | grained sand | |

The remaining two samples collected for shrink swell testing were unsuitable. Experience has shown that at times, the shrink swell index can be estimated by dividing the soil Plasticity Index (PI) by a factor of 10. The soils tested at this site have PIs of 21% and 25% which implies the shrink swell index is 2.1% and 2.5% per ΔpF .

Because there are trees and existing dwellings present, abnormal moisture conditions (AMC) prevail at the site. (Refer to Section 1.3.3 of AS2870).

Because of the AMC and low strength soils deeper than 400mm, the site is classified a Problem Site (P). It is not considered appropriate to reclassify this site.

Foundation design and construction consistent with this classification shall be adopted as specified in the above referenced standard and in accordance with the design parameters provided below.

5.2. Foundation Design

Due to the potential for differential settlements, we do not recommend founding any structural loads within in the topsoils, loose sands, and soft to firm clays.

Report No: 22/3050

Project No: 31897/6742D-G September 2022



Pad and/or strip footings founded in the stiff natural silty clays may be proportioned using an allowable bearing pressure of 100 kPa. Because of there appears to be decrease in consistency in some of the boreholes, the minimum founding depth should be 0.9 metres. The minimum depth of founding must comply with the requirements of AS2870. To overcome the presence of trees, the foundations should be designed in accordance with the procedures given in Appendices H and CH of AS2870-2011. Tree information is attached.

Piers founded in very stiff natural silty clays may be proportioned using an allowable bearing pressure of 300 kPa, provided the depth to diameter ratio exceeds a value of 4. An adhesion value of 20 kPa may be adopted below a depth of 0.5 metres.

Piers founded in weathered rock may be proportioned using an allowable end bearing pressure of 700 kPa. An allowable adhesion value of 70 kPa may be adopted for the portion of the shaft in weathered rock. When piers are founded in rock the adhesion within the overlying soils must be ignored.

During footing excavation or site preparation, weathered rock may be encountered at some locations. If this occurs, piers should be used to ensure all footings bear on materials of similar stiffness.

To ensure the bearing values given can be achieved, care should be taken to ensure that the base of excavations is free of all loose material prior to concreting. It is recommended that all shallow footing excavations be protected with a layer of blinding concrete as soon as possible, preferably immediately after excavating, cleaning, inspection, and approval. Pier excavations should not be left open overnight.

The site is considered suitable for slab on ground construction provided any loose and/or softened materials are removed and replaced with controlled engineered fill, or piers are used to suspend the slab where loose and soft to firm materials are present. The slab should be designed for movements consistent with a *Moderately Reactive (M)* classification.

During foundation construction, should the subsurface conditions vary to those inferred in this report, a suitably experienced geotechnical engineer should review the design and recommendations given above to determine if any alterations are required

5.3. Soil Aggressiveness

The aggressiveness or erosion potential of an environment in building materials, particularly concrete and steel is dependent on the levels of soil pH and the types of salts present, generally sulphates and chlorides. To determine the degree of aggressiveness, the test values obtained are compared to Tables 6.4.2 (C) and 6.5.2 (C) in AS2159 – 2009 Piling – Design and Installation. The test results are summarised in Table 5.2.

Project No: 31897/6742D-G Report No: 22/3050 Page 5

September 2022



Table 5.2– Soil Aggressiveness Summary

| Sample No. | Location | Depth (m) | рН | Sulfate (mg/kg) | Chloride (mg/kg) | Condu | trical Ictivity /m) |
|---------------|----------|--------------|-----|--------------------|---------------------|-------------------|---------------------------|
| | | | | | | EC _{1:5} | ECe |
| S1 | BH1 | 0.2 | 7.1 | <10 | <10 | 0.020 | 0.2 |
| S2 | ВН3 | 0.2 | 6.5 | <10 | <10 | 0.009 | <0.1 |
| S3 | BH5 | 0.2 | 6.5 | <10 | <10 | 0.021 | 0.2 |
| S4 | вн6 | 0.2 | 6.8 | <10 | <10 | 0.014 | 0.1 |

The soils on the site are above groundwater. Therefore, the soil conditions B are considered appropriate.

A review of the durability aspects indicates that:

• pH : minimum value of 6.5

SO₄ : maximum value of <10 mg/kg (ppm) < 5000 ppm
 Cl : maximum value of <10 mg/kg (ppm) < 5000 ppm

EC_e : maximum value of 0.2 dS/m

In accordance with AS2159-2009, the exposure classification for the onsite soils is non-aggressive to both steel and concrete. In accordance with AS2870-2011 the soils are classified as A1.

Reference to DLWC (2002) "Site Investigations for Urban Salinity" indicates that EC_e values of <0.1 to 0.2 dS/m are consistent with the presence of non-saline soils.

6. FINAL COMMENTS

During construction, should the subsurface conditions vary from those inferred above, we would be contacted to determine if any changes should be made to our recommendations. The exposed bearing surfaces for footings should be inspected by a geotechnical engineer to ensure the allowable pressure given has been achieved.

The above classification has been made assuming that all footings will bear in either natural ground or in controlled filling. Prior to the placement of any filling the existing surface should be stripped of all vegetation and topsoil.

Report No: 22/3050



If excavations for rainwater or detention tanks are to be made within 6 metres of the building foundations, advice should be sought regarding their effect on the foundations.

Placing absorption trenches on the high side of the property may create abnormal moisture conditions for the foundations (Refer to Section 1.3.3 of AS2870). This could have a negative effect on the foundation performance and more than likely alter the site classification provided above.

This report has been prepared assuming that no trees other than those noted will be present on the site. If future tree planting is planned, eg. there is a landscaping plan, their effect on the foundation performance must be considered.

This report has been prepared assuming the site development will be limited to one or two storey residential buildings. The information and interpretation may not be relevant if the design proposal changes (e.g. to a five-storey building involving major cuts during the site preparation). If changes occur, we would be pleased to review the report and advise on the adequacy of the investigation.

Page 7

Laurie Ihnativ

Senior Geotechnical Engineer

STS Geotechnics Pty Limited





Scale: Unknown

Date: August 2022

Client: NSW LAND & HOUSING CORPORATION

GEOTECHNICAL INVESTIGATION

10-16 ALBERT STREET, CASINO
BOREHOLE AND PENETROMETER LOCATIONS

Project No. 31897/6742D-G

Drawing No: 22/3050

NOTES RELATING TO GEOTECHNICAL REPORTS

Introduction

These notes have been provided to outline the methodology and limitations inherent in geotechnical reporting. The issues discussed are not relevant to all reports and further advice should be sought if there are any queries regarding any advice or report.

When copies of reports are made, they should be reproduced in full.

Geotechnical Reports

Geotechnical reports are prepared by qualified personnel on the information supplied or obtained and are based on current engineering standards of interpretation and analysis.

Information may be gained from limited subsurface testing, surface observations, previous work and is supplemented by knowledge of the local geology and experience of the range of properties that may be exhibited by the materials present. For this reason, geotechnical reports should be regarded as interpretative rather than factual documents, limited to some extent by the scope of information on which they rely.

Where the report has been prepared for a specific purpose (eg. design of a three-storey building), the information and interpretation may not be appropriate if the design is changed (eg. a twenty storey building). In such cases, the report and the sufficiency of the existing work should be reviewed by STS Geotechnics Pty Limited in the light of the new proposal.

Every care is taken with the report content, however, it is not always possible to anticipate or assume responsibility for the following conditions:

- Unexpected variations in ground conditions.
 The potential for this depends on the amount of investigative work undertaken.
- Changes in policy or interpretation by statutory authorities.
- The actions of contractors responding to commercial pressures.

If these occur, STS Geotechnics Pty Limited would be pleased to resolve the matter through further investigation, analysis or advice.

Unforeseen Conditions

Should conditions encountered on site differ markedly from those anticipated from the information contained in the report, STS Geotechnics Pty Limited should be notified immediately. Early identification of site anomalies generally results in any problems being more readily resolved and allows reinterpretation and assessment of the implications for future work.

Subsurface Information

Logs of a borehole, recovered core, test pit, excavated face or cone penetration test are an engineering and/or geological interpretation of the subsurface conditions. The reliability of the logged information depends on drilling/testing method, sampling and/or observation spacings and the ground conditions. It is not always possible or economic to obtain continuous high quality data. It should also be recognised that the volume or material observed or tested is only a fraction of the total subsurface profile.

Interpretation of subsurface information and application to design and construction must take into consideration the spacing of the test locations, the frequency of observations and testing, and the possibility that geological boundaries may vary between observation points.

Groundwater observations and measurements outside of specially designed and constructed piezometers should be treated with care for the following reasons:

- In low permeability soils groundwater may not seep into an excavation or bore in the short time it is left open.
- A localised perched water table may not represent the true water table.
- Groundwater levels vary according to rainfall events or season.
- Some drilling and testing procedures mask or prevent groundwater inflow.

The installation of piezometers and long term monitoring of groundwater levels may be required to adequately identify groundwater conditions.

Supply of Geotechnical Information or Tendering Purposes

It is recommended tenderers are provided with as much geological and geotechnical information that is available and that where there are uncertainties regarding the ground conditions, prospective tenders should be provided with comments discussing the range of likely conditions in addition to the investigation data.



APPENDIX A – BOREHOLE LOGS AND EXPLANATION SHEETS

| - | 10-16 Albert | | Date: August 17, 2022 | 1 | BOREHOLE NO.: | BH 1 |
|------------------------------------|---|------------------|---|----------------------------|--|---------------------------------|
| Location: | Refer to Draw | ving No. 22/305 | 0 Logged: AB Checked By: IW | | Sheet 1 of 1 | 1 |
| W A T T A E B R L E | S A M P L E S | DEPTH (m) | DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations) | S Y M B O L | CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels) | M O I S T U R |
| | S1 @ 0.2 m | | TOPSOIL: SILTY SANDY CLAY: brown, low plasticity | CL | - | M |
| | | 0.5 | SILTY CLAY: brown with orange, medium plasticity, some fine grained sand | CL | STIFF | M |
| | U50 | | | | | |
| | | 1.0 | SANDY SILTY CLAY: orange, trace of white, medium plasticity AUGER REFUSAL AT 1.2 M | CL | VERY STIFF | M |
| | D - disturbed WT - level of S - jar sampl | f water table or | | Hole Dian | nt: Christie neter (mm): 100 | <u> </u> |
| NOTES: | | | See explanation sheets for meaning of all descriptive terms and symbols | Angle from | n Vertical (°): 0 Spiral | |

GEOTECHNICAL LOG - NON CORE BOREHOLE

| Client: | NSW Land & 10-16 Albert | Housing Corpor | ation Project / STS No. 31897/6742D-G Date: August 17, 2022 | В | OREHOLE NO.: | BH 2 |
|------------------------|--|---------------------|---|----------------------------|--|-----------------|
| II . | | ving No. 22/305 | | | Sheet 1 of 1 | |
| W ATTA EBRL E | S A M P L E S | DEPTH (m) | DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations) | S Y M B O L | CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels) | M O I S T U R E |
| | | | TOPSOIL: SILTY CLAY: brown, low plasticity | CL | - | D-M |
| | | 0.5 | CLAYEY SILTY SAND: dark grey | SM | MEDIUM DENSE | W |
| | | | SILTY CLAY: grey with orange, medium plasticity | CL | FIRM | М |
| | | 1.0 | SANDY CLAY: dark grey SILTY CLAY: orange, medium plasticity | SC CL | SOFT TO FIRM | W M-D |
| | | 1.5 | | | VERY STIFF | |
| | | 2.0 | WEATHERED ROCK: white AUGER REFUSAL AT 1.7 M ON WEATHERED ROCK | | EXTREMELY LOW STRENGTH | D |
| | | 2.0 | | | | |
| NOTES: | D - disturber WT - level o S - jar sampl | f water table or | free water N - Standard Penetration Test (SPT) See explanation sheets for meaning of all descriptive terms and symbols | Hole Diam | t: Christie eter (mm): 100 Vertical (°): 0 | |

Revision: 1

| | | Housing Corpor Street, Casino | ation Project / STS No. 31897/6742D-G Date: August 17, 2022 | В | OREHOLE NO.: | BH 3 |
|-----------------------|--|----------------------------------|---|----------------------------|--|-----------------|
| _ | | ving No. 22/305 | | | Sheet 1 of 1 | |
| W ATTA EB RL | S A M P L E S | DEPTH (m) | DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations) | S Y M B O L | consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels) | M O I S T U R E |
| | | | TOPSOIL: SILTY CLAY: brown, low plasticity | CL | - | D-M |
| | S2 @ 0.2 m | 0.5 | CLAYEY SAND: grey brown, some silt | CS | LOOSE | W |
| | U50 | | SILTY CLAY: grey with orange, medium plasticity | CL | SOFT TO FIRM STIFF | М |
| | | 1.0 | AUGER REFUSAL AT 1.0 M | | | |
| No. | D - disturbe WT - level o S - jar samp | f water table or | free water N - Standard Penetration Test (SPT) | Iole Diam | t: Christie eter (mm): 100 Vertical (°): 0 | |
| NOTES: | | | | orill Bit: S | | |

| Location: Refer to Drawing No. 22/3050 Logged: A8 Checked By: W Shipper | | | Housing Corpor | project / STS No. 31897/6742D-G Date: August 17, 2022 | В | OREHOLE NO.: | BH 4 |
|--|----------|-----------------------|------------------|--|----------------------|--|---------------------------------|
| A T A A A S S Y N S S S S S S S S S S S S S S S S | | | | | | Sheet 1 of 1 | |
| TOPSOIL SILTY CLAY: brown, low platticity SILTY CLAY: orange brown, medium plasticity CL FII SILTY CLAY: orange brown, medium plasticity CL FII WEATHERED ROCK: white orange ALIGER REFUSAL AT 1.4 M ON WEATHERED ROCK 1.5 2.0 2.0 | ATTAEBRL | A M P L E | | | Y M B | consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels) | M O I S T U R |
| SILTY CLAY: orange brown, medium plasticity C.L. FIII 1.0 | | | | TOPSOIL: SILTY CLAY: brown, low plasticity | | - | D-M |
| 1.0 WEATHERED ROCK: white orange WEATHERED ROCK AUGER REFUSAL AT 1.4 M ON WEATHERED ROCK 1.5 2.0 2.0 | | | | SILTY CLAYEY SAND: grey brown | SM | LOOSE | W |
| WEATHERED ROCK: white orange AUGER REFUSAL AT 1.4 M ON WEATHERED ROCK 2.0 2.0 2.0 | | | 0.5 | SILTY CLAY: orange brown, medium plasticity | CL | FIRM TO STIFF | M |
| 2.0 | | | | WEATHERED ROCK: white orange | | VERY STIFF EXTREMELY LOW | D |
| | | | 2.0 | AUGER REFUSAL AT 1.4 M ON WEATHERED ROCK | | STRENGTH | |
| D - disturbed sample U - undisturbed tube sample B - bulk sample Contractor: STS WT - level of water table or free water N - Standard Penetration Test (SPT) Equipment: Chri S - jar sample NOTES: See explanation sheets for meaning of all descriptive terms and symbols Angle from Vertica Drill Bit: Spiral | NOTES: | WT - level of | f water table or | free water N - Standard Penetration Test (SPT) Free water N - Standard Penetration Test (SPT) | quipmen Hole Diam | t: Christie eter (mm): 100 Vertical (°): 0 | |

| | NSW Land & 10-16 Albert | _ | | project / STS No. 31897/6742D-G Date: August 17, 2022 | E | BOREHOLE NO.: | BH 5 |
|------------------------|--|-------------------------------|---|--|----------------------------|--|-----------------|
| | Refer to Draw | | | | | Sheet 1 of 1 | |
| W ATTA EBRL E | S A M P L E S | DEP [*] (m | | DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations) | S Y M B O L | CONSISTENCY (cohesive soils) or RELATIVE DENSITY (sands and gravels) | M O I S T U R E |
| | | | | TOPSOIL: SILTY CLAY: brown, low plasticity | CL | - | D-M |
| | S3 @ 0.2 m | 0.5 | _ | SILTY CLAYEY SAND: brown, some gravel | SM | LOOSE | W |
| | | 1.0 | _ | SILTY CLAY: brown mottled orange, medium plasticity | CL | VERY STIFF | М |
| | | - 1.5 _ - - | | WEATHERED ROCK: white orange | | EXTREMELY LOW STRENGTH | D |
| | | 2.0 _ | | AUGER REFUSAL AT 2.0 M ON WEATHERED ROCK | | | |
| NOTES: | D - disturber WT - level o S - jar sampl | f water ta | | free water N - Standard Penetration Test (SPT) For example 1 See explanation sheets for meaning of all descriptive terms and symbols A | Iole Diam | t: Christie leter (mm): 100 n Vertical (°): 0 | ı |

| Client: Project: | NSW Land & Housing Corporat 10-16 Albert Street, Casino | | | ation Project / STS No. 31897/6742D-G Date: August 17, 2022 | В | OREHOLE NO.: | ВН 6 |
|-----------------------|--|--------|------------------|---|----------------------------|--|-----------------|
| | Refer to Draw | | | | | Sheet 1 of 1 | |
| W ATTA EB RL | S A M P L E S | | PTH m) | DESCRIPTION OF DRILLED PRODUCT (Soil type, colour, grain size, plasticity, minor components, observations) | S Y M B O L | consistency (cohesive soils) or RELATIVE DENSITY (sands and gravels) | M O I S T U R E |
| | | | <u> </u> | TOPSOIL: SILTY CLAY: brown, low plasticity | CL | - | D-M |
| | S4 @ 0.2 m | 0.5 | | CLAYEY SILTY SAND: grey | SM | LOOSE TO MEDIUM DENSE | W |
| | | 0.5 | | SILTY CLAY: orange mottled grey, medium plasticity | CL | FIRM TO STIFF | M |
| | U50 | 1.0 | | | | | |
| | | 1.5 | | SILTY CLAY: grey, medium plasticity | CL | VERY STIFF | М |
| | | 2.0 | | WEATHERED ROCK: orange AUGER REFUSAL AT 2.2 M ON WEATHERED ROCK | | EXTREMELY LOW STRENGTH | D-M |
| NOTES: | D - disturbe WT - level o S - jar sampl | fwater | | free water N - Standard Penetration Test (SPT) Free explanation sheets for meaning of all descriptive terms and symbols All | Iole Diam | t: Christie eter (mm): 100 Vertical (°): 0 | |



14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Report No.: 22/3049

Dynamic Cone Penetrometer Test Report

Project: 10-16 ALBERT STREET, CASINO Project No.: 31897/6742D

Client: NSW LAND & HOUSING CORPORATION

Address: Level G, 12 Darcy Street, Parramatta Report Date: August 22, 2022

Test Method: AS 1289.6.3.2 Page: 1 of 1

| Site No. | P1 | P2 | P3 | P4 | P5 | P6 |
|----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| Location | Refer to Drawing No. 22/3050 |
| Date Tested | 17/8/2022 | 17/8/2022 | 17/8/2022 | 17/8/2022 | 17/8/2022 | 17/8/2022 |
| Starting Level | Surface Level | Surface Level | Surface Level | Surface Level | Surface Level | Surface Level |
| Depth (m) | | Pe | netration Resistar | nce (blows / 150m | m) | |
| 0.00 - 0.15 | 5 | 3 | 1 | 2 | 1 | 1 |
| 0.15 - 0.30 | 7 | 4 | 3 | 2 | 1 | 3 |
| 0.30 - 0.45 | 5 | 4 | 2 | 3 | 2 | 3 |
| 0.45 - 0.60 | 4 | 5 | 2 | 3 | 2 | 3 |
| 0.60 - 0.75 | 5 | 3 | 1 | 2 | 9 | 3 |
| 0.75 - 0.90 | 4 | 2 | 5 | 3 | 21 | 3 |
| 0.90 - 1.05 | 15 | 5 | 8 | 4 | 23 | 4 |
| 1.05 - 1.20 | Refusal | 8 | 13 | 5 | Refusal | 5 |
| 1.20 - 1.35 | | 13 | 23 | 21 | | 15 |
| 1.35 - 1.50 | | 23 | 23 | 10 | | 22 |
| 1.50 - 1.65 | | 23 | Refusal | Refusal | | 23 |
| 1.65 - 1.80 | | Refusal | | | | Refusal |
| 1.80 - 1.95 | | | | | | |
| 1.95 - 2.10 | | | | | | |
| 2.10 - 2.25 | | | | | | |
| 2.25 - 2.40 | | | | | | |
| 2.40 - 2.55 | | | | | | |
| 2.55 - 2.70 | | | | | | |
| 2.70 - 2.85 | | | | | | |
| 2.85 - 3.00 | | | | | | |
| 3.00 - 3.15 | | | | | | |
| 3.15 - 3.30 | | | | | | |
| 3.30 - 3.45 | | | | | | |
| 3.45 - 3.60 | | | | | | |
| 3.60 - 3.75 | | | | | | |

Remarks: * Pre drilled prior to testing

ΑB

Technician:

Approved Signatory.....

Orlando Mendoza - Laboratory Manager

Form: RPS26 Date of Issue: 31/05/21 Revision: 2

E1. CLASSIFICATION OF SOILS

E1.1 Soil Classification and the Unified System

An assessment of the site conditions usually includes an appraisal of the data available by combining values of engineering properties obtained by the site investigation with descriptions, from visual observation of the materials present on site.

The system used by STS Geotechnics Pty Ltd (STS) in the identification of soil is the Unified Soil Classification system (USC) which was developed by the US Army Corps of Engineers during World War II and has since gained international acceptance and has been adopted in its metricated form by the Standards Association of Australia.

The Australian Site Investigation Code (AS1726-2017, Appendix D) recommends that the description of a soil includes the USC group symbols which are an integral component of the system.

The soil description should contain the following information in order:

Soil composition

- SOIL NAME and USC classification symbol (IN BLOCK LETTERS)
- plasticity or particle characteristics
- colour
- secondary and minor constituents (name estimated proportion, plasticity or particle characteristics, colour

Soil condition

- moisture condition
- consistency or density index

Soil structure

• structure (zoning, defects, cementing)

Soil origin

interpretation based on observation eg FILL, TOPSOIL, RESIDUAL, ALLUVIUM.

E1.2 Soil Composition

(a) Soil Name and Classification Symbol

The USC system is summarised in Figure E1.2.1. The primary division separates soil types on the basis of particle size into:

- Coarse grained soils more than 50% of the material less than 60 mm is larger than 0.06 mm (60 μm).
- Fine grained soils more than 50% of the material less than 60 mm is smaller than 0.06 mm (60 μ m).

Initial classification is by particle size as shown in Table E1.2.1. Further classification of fine grained soils is based on plasticity.

TABLE E1.2.1 - CLASSIFICATION BY PARTICLE SIZE

| NAME | SUB-DIVISION | SIZE |
|--------------|--------------------------|---|
| Clay (1) | | < 2 μm |
| Silt (2) | | 2 μm to 60 μm |
| Sand | Fine Medium Coarse | 60 μm to 200 μm 200 μm to 600 μm 600 μm to 2 mm |
| Gravel (3) | Fine Medium Coarse | 2 mm to 6 mm 6 mm to 20 mm 20 mm to 60 mm |
| Cobbles (3) | | 60 mm to 200 mm |
| Boulders (3) | | > 200 mm |

Where a soil contains an appropriate amount of secondary material, the name includes each of the secondary components (greater than 12%) in increasing order of significance, eg sandy silty clay.

Minor components of a soil are included in the description by means of the terms "some" and "trace" as defined in Table E1.2.2.

TABLE E1.2.2 - MINOR SOIL COMPONENTS

| TERM | DESCRIPTION | APPROXIMATE PROPORTION (%) |
|-------|--|-------------------------------|
| Trace | presence just detectable, little or no influence on soil properties | 0-5 |
| Some | presence easily detectable, little influence on soil properties | 5-12 |

The USC group symbols should be included with each soil description as shown in Table E1.2.3

TABLE E1.2.3 - SOIL GROUP SYMBOLS

| SOIL TYPE | PREFIX |
|-----------|--------|
| Gravel | G |
| Sand | S |
| Silt | M |
| Clay | С |
| Organic | 0 |
| Peat | Pt |

The group symbols are combined with qualifiers which indicate grading, plasticity or secondary components as shown on Table E1.2.4

TABLE E1.2.4 - SOIL GROUP QUALIFIERS

| SUBGROUP | SUFFIX |
|---|--------|
| Well graded | W |
| Poorly Graded | P |
| Silty | M |
| Clayey | C |
| Liquid Limit <50% - low to medium plasticity | L |
| Liquid Limit >50% - medium to high plasticity | Н |

(b) Grading

"Well graded" Good representation of all

particle sizes from the largest

to the smallest.

"Poorly graded" One or more intermediate

sizes poorly represented

"Gap graded" One or more intermediate

sizes absent

"Uniformly graded" Essentially single size

material.

(c) Particle shape and texture

The shape and surface texture of the coarse grained particles should be described.

Angularity may be expressed as "rounded", "subrounded", "sub-angular" or "angular".

Particle **form** can be "equidimensional", "flat" or elongate".

Surface texture can be "glassy", "smooth", "rough", pitted" or striated".

(d) Colour

The colour of the soil should be described in the moist condition using simple terms such as:

Black White Grey Red Brown Orange Yellow Green Blue

These may be modified as necessary by "light" or "dark". Borderline colours may be described as a combination of two colours, eg red-brown.

For soils that contain more than one colour terms such as:

• Speckled Very small (<10 mm dia) patches

• Mottled Irregular

• Blotched Large irregular (>75 mm dia)

• Streaked Randomly oriented streaks

(e) Minor Components

Secondary and minor components should be individually described in a similar manner to the dominant component.

E1.3 Soil Condition

(a) Moisture

Soil moisture condition is described as "dry", "moist" or "wet".

The moisture categories are defined as:

Dry (D) - Little or no moisture evident. Soils are running. Moist (M) - Darkened in colour with cool feel. Granular soil particles tend to adhere. No free water evident upon remoulding of cohesive soils.

In addition the moisture content of cohesive soils can be estimated in relation to their liquid or plastic limit.

(b) Consistency

Estimates of the consistency of a clay or silt soil may be made from manual examination, hand penetrometer test, SPT results or from laboratory tests to determine undrained shear or unconfined compressive strengths. The classification of consistency is defined in Table E1.3.1.

TABLE E1.3.1 - CONSISTENCY OF FINE-GRAINED SOILS

| TERM | UNCONFINED STRENGTH (kPa) | FIELD IDENTIFICATION |
|---------------|---------------------------------|--|
| Very Soft | <25 | Easily penetrated by fist. Sample exudes between fingers when squeezed in the fist. |
| Soft | 25 - 50 | Easily moulded in fingers. Easily penetrated 50 mm by thumb. |
| Firm | 50 - 100 | Can be moulded by strong pressure in the fingers. Penetrated only with great effort. |
| Stiff | 100 - 200 | Cannot be moulded in fingers. Indented by thumb but penetrated only with great effort. |
| Very Stiff | 200 - 400 | Very tough. Difficult to cut with knife. Readily indented with thumb nail. |
| Hard | >400 | Brittle, can just be scratched with thumb nail. Tends to break into fragments. |

Unconfined compressive strength as derived by a hand penetrometer can be taken as approximately double the undrained shear strength $(q_u = 2 \ c_u)$.

(c) Density Index

The insitu density index of granular soils can be assessed from the results of SPT or cone penetrometer tests. Density index should not be estimated visually.

TABLE E1.3.2 - DENSITY OF GRANULAR SOILS

| TERM | SPT N | STATIC | DENSITY |
|--------------|---------|----------------------|---------|
| | VALUE | CONE | INDEX |
| | | VALUE | (%) |
| | | q _c (MPa) | |
| Very Loose | 0 - 3 | 0 - 2 | 0 - 15 |
| Loose | 3 - 8 | 2 - 5 | 15 - 35 |
| Medium Dense | 8 - 25 | 5 - 15 | 35 - 65 |
| Dense | 25 - 42 | 15 - 20 | 65 - 85 |
| Very Dense | >42 | >20 | >85 |

E1.4 Soil Structure

(a) Zoning

A sample may consist of several zones differing in colour, grain size or other properties. Terms to classify these zones are:

Layer - continuous across exposure or sample

Lens - discontinuous with lenticular shape

Pocket - irregular inclusion

Each zone should be described, their distinguishing features, and the nature of the interzone boundaries.

(b) Defects

Defects which are present in the sample can include:

- fissures
- roots (containing organic matter)
- tubes (hollow)
- · casts (infilled)

Defects should be described giving details of dimensions and frequency. Fissure orientation, planarity, surface condition and infilling should be noted. If there is a tendency to break into blocks, block dimensions should be recorded

E1.5 Soil Origin

Information which may be interpretative but which may contribute to the usefulness of the material description should be included. The most common interpreted feature is the origin of the soil. The assessment of the probable origin is based on the soil material description, soil structure and its relationship to other soil and rock materials.

Common terms used are:

"Residual Soil" - Material which appears to have been derived by weathering from the underlying rock. There is no evidence of transport.

"Colluvium" - Material which appears to have been transported from its original location. The method of movement is usually the combination of gravity and erosion

"Landslide Debris" - An extreme form of colluvium where the soil has been transported by mass movement. The material is obviously distributed and contains distinct defects related to the slope failure.

"Alluvium" - Material which has been transported essentially by water. usually associated with former stream activity.

"Fill" - Material which has been transported and placed by man. This can range from natural soils which have been placed in a controlled manner in engineering construction to dumped waste material. A description of the constituents should include an assessment of the method of placement.

E1.6 Fine Grained Soils

The physical properties of fine grained soils are dominated by silts and clays.

The definition of clay and silt soils is governed by their Atterberg Limits. Clay soils are characterised by the properties of cohesion and plasticity with cohesion defines as the ability to deform without rupture. Silts exhibit cohesion but have low plasticity or are non-plastic.

The field characteristics of clay soils include:

- dry lumps have appreciable dry strength and cannot be powdered
- volume changes occur with moisture content variation
- feels smooth when moist with a greasy appearance when cut.

The field characteristics of silt soils include:

- dry lumps have negligible dry strength and can be powdered easily
- dilatancy an increase in volume due to shearing is indicted by the presence of a shiny film of water after a hand sample is shaken. The water disappears upon remoulding. Very fine grained sands may also exhibit dilatancy.
- low plasticity index
- · feels gritty to the teeth

E1.7 Organic Soils

Organic soils are distinguished from other soils by their appreciable content of vegetable matter, usually derived from plant remains.

The soil usually has a distinctive smell and low bulk density.

The USC system uses the symbol Pt for partly decomposed organic material. The O symbol is combined with suffixes "O" or "H" depending on plasticity.

Where roots or root fibres are present their frequency and the depth to which they are encountered should be recorded. The presence of roots or root fibres does not necessarily mean the material is an "organic material" by classification.

Coal and lignite should be described as such and not simply as organic matter.



APPENDIX B - LABORATORY TEST RESULTS



14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Shrink Swell Index Report

Project: 10-16 ALBERT STREET, CASINO
Project No.: 31897

Client: NSW LAND & HOUSING CORPORATION
Address: Level G, 12 Darcy Street, Parramatta
Report Date: 26/08/2022

Test Method: AS1289.7.1.1
Page: 1 OF 1

Sampling Procedure: AS 1289.1.3.1 Clause 3.1.3.2 - Thin Walled Sampler

| | | | | | |
|----------------------|---------------------------------|--|------|------|--|
| STS | / Sample No. | 6742D-L/1 | | | |
| Sample Location | | Borehole 1 Refer to Drawing No. 22/3050 | | | |
| Material Description | | Silty Sandy Clay, grey brown/blue | | | |
| [| Depth (m) | 0.7 - 0.9 | | | |
| Sa | ample Date | 17/08/2022 | | | |
| | Moisture Content (%) | 17.3 | | | |
| Shrink | Soil Crumbling | Nil | | | |
| Shr | Extent of Cracking | Nil | | | |
| | Strain (%) | 3.7 | | | |
| | Moisture Content Initial (%) | 19.3 | | | |
| Swell | Moisture Content Final (%) | 32.3 | | | |
| | Strain (%) | 0.0 | | | |
| Inert | Inclusions (%) | <5 | | | |
| Shrink | Swell Index (%) | 2.0 | | | |

Remarks:

Approved Signatory.....

Orlando Mendoza - Laboratory Manager

Revision: 2

Technician: AW

GEOTECHNICS PTY LTD

STS Geotechnics Pty Ltd

14/1 Cowpasture Place, Wetherill Park NSW 2164 Phone: (02)9756 2166 | Email: enquiries@stsgeo.com.au



Atterberg Limits and Linear Shrinkage Report

Project: 10 - 16 ALBERT STREET, CASINO Project No.: 31897

Client: NSW LAND & HOUSING CORPORATION

Report No.: 22/3202

Address: Level G, 12 Darcy Street, Parramatta 2150

Report Date: 5/09/2022

Test Method: AS1289.3.1.2,3.2.1,3.4.1,2.1.1 Page: 1 OF 1

Sampling Procedure: AS 1289.1.2.1 Clause 6.5.3 - Power Auger Drilling (Not covered under NATA Scope of Accreditation)

| STS / Sample No. | 6742D-L / 2 | 6742D-L/3 | | |
|--------------------------|---|---|--|--|
| Sample Location | Borehole 3, Refer to Drawing No. 22/3050 | Borehole 6, Refer to Drawing No. 22/3050 | | |
| Material Description | Sandy Clay, grey | Sandy Clay, grey brown | | |
| Depth (m) | 0.8 - 1.0 | 0.7 - 0.9 | | |
| Sample Date | 17/08/2022 | 17/08/2022 | | |
| Sample History | Oven Dried | Oven Dried | | |
| Method of Preparation | Dry Sieved | Dry Sieved | | |
| Liquid Limit (%) | 21 | 46 | | |
| Plastic Limit (%) | 20 | 21 | | |
| Plasticity Index | 21 | 25 | | |
| Linear Shrinkage (%) | 12.5 | 14.0 | | |
| Mould Size (mm) | 127.00 | 127.13 | | |
| Crumbing | N | N | | |
| Curling | N | N | | |

Remarks:

Approved Signatory.....

Technician: AW Orlando Mendoza - Laboratory Manager

Form RPS13 Date of Issue: 31/05/21 Revision: 2



CERTIFICATE OF ANALYSIS

Work Order : ES2229925

Page : 1 of 8

Contact : Enquiries

Client

Telephone

Quote number

No. of samples analysed

Laboratory : Environmental Division Sydney

Address : Unit 14/1 Cowpasture Place

Contact : Customer Services ES

Address : 277-289 Woodpark Road Smithfield NSW Australia 2164

Wetherill Park 2164

Telephone : +61-2-8784 8555

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924

: STS Geotechnics

Date Samples Received : 22-Aug-2022 17:50

Order number : 2022-271

Date Analysis Commenced : 23-Aug-2022

C-O-C number · ----

Date / mary sis commenced . 23-Aug-20

Sampler ; AB, EJ, MB

Issue Date

: 25-Aug-2022 12:55

Site · ---

: ----

: EN/222

No. of samples received : 26

: 26

Accredited for a second second

Accreditation No. 825
Accredited for compliance with
ISO/IEC 17025 - Testing

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with Quality Review and Sample Receipt Notification.

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories Position Accreditation Category

Ankit Joshi Senior Chemist - Inorganics Sydney Inorganics, Smithfield, NSW

Page : 2 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contract for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.

LOR = Limit of reporting

- ^ = This result is computed from individual analyte detections at or above the level of reporting
- ø = ALS is not NATA accredited for these tests.
- ~ = Indicates an estimated value.

Page : 3 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



| Sub-Matrix: SOIL (Matrix: SOIL) | | | Sample ID | 30055/8551 | 30055/8552 | 30055/8553 | 30055/8554 | 30055/8555 |
|---------------------------------------|------------|--------|----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | | Sampli | ng date / time | 19-Aug-2022 00:00 |
| Compound | CAS Number | LOR | Unit | ES2229925-001 | ES2229925-002 | ES2229925-003 | ES2229925-004 | ES2229925-005 |
| | | | | Result | Result | Result | Result | Result |
| EA002: pH 1:5 (Soils) | | | | | | | | |
| pH Value | | 0.1 | pH Unit | 7.3 | 7.2 | 6.8 | 6.5 | 6.8 |
| EA010: Conductivity (1:5) | | | | | | | | |
| Electrical Conductivity @ 25°C | | 1 | μS/cm | 11 | 68 | 44 | 19 | 54 |
| EA055: Moisture Content (Dried @ 105- | 110°C) | | | | | | | |
| Moisture Content | | 0.1 | % | 6.5 | 17.8 | 15.1 | 13.8 | 13.2 |
| ED040S : Soluble Sulfate by ICPAES | | | | | | | | |
| Sulfate as SO4 2- | 14808-79-8 | 10 | mg/kg | <10 | 70 | <10 | <10 | 10 |

Page : 4 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



| Sub-Matrix: SOIL (Matrix: SOIL) | | | Sample ID | 30055/8556 | 31354/087 | 31354/088 | 31894/S1 | 31894/S2 |
|--------------------------------------|------------|--------|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | | Sampli | ing date / time | 19-Aug-2022 00:00 |
| Compound | CAS Number | LOR | Unit | ES2229925-006 | ES2229925-007 | ES2229925-008 | ES2229925-009 | ES2229925-010 |
| | | | | Result | Result | Result | Result | Result |
| EA002: pH 1:5 (Soils) | | | | | | | | |
| pH Value | | 0.1 | pH Unit | 6.1 | 6.0 | 6.9 | 7.4 | 7.0 |
| EA010: Conductivity (1:5) | | | | | | | | |
| Electrical Conductivity @ 25°C | | 1 | μS/cm | 106 | 160 | 117 | 32 | 25 |
| EA055: Moisture Content (Dried @ 105 | 5-110°C) | | | | | | | |
| Moisture Content | | 0.1 | % | 14.4 | 22.8 | 23.0 | 5.9 | 7.1 |
| ED040S : Soluble Sulfate by ICPAES | | | | | | | | |
| Sulfate as SO4 2- | 14808-79-8 | 10 | mg/kg | 40 | 210 | 60 | <10 | <10 |
| ED045G: Chloride by Discrete Analyse | er | | | | | | | |
| Chloride | 16887-00-6 | 10 | mg/kg | | | | 30 | 50 |

Page : 5 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



| Sub-Matrix: SOIL (Matrix: SOIL) | | | Sample ID | 31894/S3 | 31894/S4 | 31895/S1 | 31895/S2 | 31896/S1 |
|---|----------------------|-----|-----------|---------------|---------------|-------------------|-------------------|-------------------|
| | Sampling date / time | | | | | 19-Aug-2022 00:00 | 19-Aug-2022 00:00 | 19-Aug-2022 00:00 |
| Compound | CAS Number | LOR | Unit | ES2229925-011 | ES2229925-012 | ES2229925-013 | ES2229925-014 | ES2229925-015 |
| | | | | Result | Result | Result | Result | Result |
| EA002: pH 1:5 (Soils) | | | | | | | | |
| pH Value | | 0.1 | pH Unit | 6.4 | 6.2 | 5.8 | 6.3 | 7.1 |
| EA010: Conductivity (1:5) | | | | | | | | |
| Electrical Conductivity @ 25°C | | 1 | μS/cm | 37 | 61 | 68 | 25 | 43 |
| EA055: Moisture Content (Dried @ 105-11 | 10°C) | | | | | | | |
| Moisture Content | | 0.1 | % | 13.8 | 22.4 | 10.4 | 11.9 | 12.3 |
| ED040S : Soluble Sulfate by ICPAES | | | | | | | | |
| Sulfate as SO4 2- | 14808-79-8 | 10 | mg/kg | 20 | 20 | 90 | <10 | 30 |
| ED045G: Chloride by Discrete Analyser | | | | | | | | |
| Chloride | 16887-00-6 | 10 | mg/kg | 130 | 60 | <10 | 20 | <10 |

Page : 6 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



| Sub-Matrix: SOIL (Matrix: SOIL) | | | Sample ID | 31896/S2 | 31896/\$3 | 31897/S1 | 31897/S2 | 31897/\$3 |
|--|------------|--------|----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | | Sampli | ng date / time | 19-Aug-2022 00:00 |
| Compound | CAS Number | LOR | Unit | ES2229925-016 | ES2229925-017 | ES2229925-018 | ES2229925-019 | ES2229925-020 |
| | | | | Result | Result | Result | Result | Result |
| EA002: pH 1:5 (Soils) | | | | | | | | |
| pH Value | | 0.1 | pH Unit | 6.9 | 7.0 | 7.1 | 6.5 | 6.5 |
| EA010: Conductivity (1:5) | | | | | | | | |
| Electrical Conductivity @ 25°C | | 1 | μS/cm | 17 | 31 | 20 | 9 | 21 |
| EA055: Moisture Content (Dried @ 105-1 | 10°C) | | | | | | | |
| Moisture Content | | 0.1 | % | 15.2 | 13.4 | 7.4 | 10.4 | 11.4 |
| ED040S : Soluble Sulfate by ICPAES | | | | | | | | |
| Sulfate as SO4 2- | 14808-79-8 | 10 | mg/kg | <10 | <10 | <10 | <10 | <10 |
| ED045G: Chloride by Discrete Analyser | | | | | | | | |
| Chloride | 16887-00-6 | 10 | mg/kg | <10 | 20 | <10 | <10 | <10 |

Page : 7 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



| Sub-Matrix: SOIL (Matrix: SOIL) | | | Sample ID | 31897/S4 | 31911/S1 | 31913/S1 | 31913/S2 | 31913/\$3 |
|--|------------|--------|----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | | Sampli | ng date / time | 19-Aug-2022 00:00 |
| Compound | CAS Number | LOR | Unit | ES2229925-021 | ES2229925-022 | ES2229925-023 | ES2229925-024 | ES2229925-025 |
| | | | | Result | Result | Result | Result | Result |
| EA002: pH 1:5 (Soils) | | | | | | | | |
| pH Value | | 0.1 | pH Unit | 6.8 | 5.4 | 5.5 | 5.9 | 4.4 |
| EA010: Conductivity (1:5) | | | | | | | | |
| Electrical Conductivity @ 25°C | | 1 | μS/cm | 14 | 25 | 27 | 28 | 96 |
| EA055: Moisture Content (Dried @ 105-1 | 10°C) | | | | | | | |
| Moisture Content | | 0.1 | % | 10.1 | 29.5 | 22.0 | 25.8 | 22.7 |
| ED040S : Soluble Sulfate by ICPAES | | | | | | | | |
| Sulfate as SO4 2- | 14808-79-8 | 10 | mg/kg | <10 | 30 | <10 | <10 | 50 |
| ED045G: Chloride by Discrete Analyser | | | | | | | | |
| Chloride | 16887-00-6 | 10 | mg/kg | <10 | 10 | 20 | 20 | 20 |

Page : 8 of 8
Work Order : ES2229925

Client : STS Geotechnics

Project : 30055/31354/31894/31895/31896/31897/31911/31913/31924



| Sub-Matrix: SOIL (Matrix: SOIL) | | | Sample ID | 31924/S1 | | | |
|---|----------------------|-----|-----------|---------------|--|------|--|
| | Sampling date / time | | | | | | |
| Compound | CAS Number | LOR | Unit | ES2229925-026 | | | |
| | | | | Result | | | |
| EA002: pH 1:5 (Soils) | | | | | | | |
| pH Value | | 0.1 | pH Unit | 5.8 | | | |
| EA010: Conductivity (1:5) | | | | | | | |
| Electrical Conductivity @ 25°C | | 1 | μS/cm | 22 | | | |
| EA055: Moisture Content (Dried @ 105-11 | 10°C) | | | | | | |
| Moisture Content | | 0.1 | % | 24.7 | | | |
| ED040S : Soluble Sulfate by ICPAES | | | | | | | |
| Sulfate as SO4 2- | 14808-79-8 | 10 | mg/kg | <10 | | | |
| ED045G: Chloride by Discrete Analyser | | | | | | | |
| Chloride | 16887-00-6 | 10 | mg/kg | <10 | | | |